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# Cross Laminated Timber (CLT) in Europe: Resistance against Fire



Cross Laminated Timber (CLT) Fire Performance Workshop Canadian Wood Councils

Univ.-Prof. Dipl.-Ing. Dr.techn. Gerhard Schickhofer Institute for Timber Engineering and Wood Technology, Graz University of Technology | AT Competence Centre holz.bau forschungs gmbh Graz | AT

Gerhard Schickhofer

Vancouver, Canada, 23rd March 2010



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- "TIMBER" at the Graz University of Technology
  - Institute for Timber Engineering and Wood Technology (TEWT)
  - Competence Centre holz.bau forschungs gmbh (hbf)
  - R&D Areas
- Cross Laminated Timber and Fire
  - Motivation for Research on Fire-resistance of CLT
  - Introduction | History
  - Research Project hbf TUG ETHZ
  - Future Developments
- Summary



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# **GRAZ UNIVERSITY OF TECHNOLOGY**

Austria / Europe 7 faculties | 11,264 students | staff 2,222 budget: € 150 Mill. (1/3 3<sup>rd</sup> party budget)

# **Faculty of Civil Engineering Sciences**

**17 institutes | about 1,140 students** [207 "diploma", 693 "Bachelor", 146 "Master", 93 "PhD"]

# Institute for Timber Engineering and Wood Technology

1991: Chair for Timber Engineering

10|2004: Institute Timber Engineering and Wood Technology

Scientific staff: 7.0 FTE | third-party-budget: € 250.000 (2008)

### Competence Centre holz.bau forschungs gmbh

- 09|2002 Acceptance of <u>4-year-fundings:</u> Competence Center Timber Engineering and Wood Technology
- 12|2002 Competence Centre holz.bau forschungs gmbh
- 09|2007 Acceptance of <u>5-year-fundings:</u> K-Project "timber.engineering" | COMET-Programme

Scientific staff: **7.1 FTE** | budget: € **1.000.000** (2008)







## AREA 1 Timber Engineering (TE) – Design and Construction Sciences (DCS)

### 1.1 Shell and Spatial Timber Constructions (SSTC)



#### \_\_\_\_\_

1.2 Innovative and Intelligent Connection Systems (IICS)



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## AREA 2 Wood Technology (WT) – Material and Structure Sciences (MSS)

## 2.1 Advanced Products and Test Methods (APTM)



### 2.2 Material Modelling and Simulation Methods (MMSM)



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### EN 1995-1-2:2006

Design of timber structures - Part 1-2\_General - Structural fire design.pdf

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	Y	

Table 3.1 – Design charring rates $\beta_0$ and $\beta_n$ of timber, LVL, wood panelling and wood-
based panels

	β₀ mm/min	β <sub>n</sub> mm/min
<ul> <li>a) Softwood and beech</li> <li>Glued laminated timber with a characteristic density of ≥ 290 kg/m<sup>3</sup></li> <li>Solid timber with a characteristic density of ≥ 290 kg/m<sup>3</sup></li> </ul>	0,65 0,65	0,7 0,8 because of cracks

 $\beta_0 \dots$  design charring rate for one-dimensional under standard fire exposure

 $\beta_n \dots$  is the notional design charring rate, the magnitude of which includes the effect of corner roundings and fissures

# **Cross Laminated Timber CLT**

- Wide spanned, multi-layered wood based product
- Strength graded board as base product
- Orthogonally glued layers



- Up to now CLT is not regulated within the design standard!
- Assumption: if the base-material "board" and the board-based product GLT have the same charring rate  $\beta_0$

 $\Rightarrow$  than the board-based product CLT also has the

same charring rate







## Signs of need for research

1. Research Project ETH Zürich (Technical Report published 2007)

"...single layers of 3-layer-boards fell off after burn-through ... it can be assumed that claddings with layered cross sections, e.g. 3-layer-boards, have an disadvantageous behaviour compared to solid timber boards."

2. European Technical Approval ETA from a producer (2007)

Resistance to fire		
<ul> <li>Charring rate, see Annex 4</li> <li>Charring of cover layer only.</li> <li>The cross section of the remaining wood shall be reduced by 10 %.</li> <li>At least 3 mm of the cover layer shall remain unchared.</li> </ul>	EN 1995-1-2	0,67 mm/min
<ul> <li>Charring of more layers than the cover layer.</li> </ul>		0,76 mm/min



# **Research on Fire behaviour of CLT**

- 1. Bresta H KLH (1998): fire-bending tests on loaded 5-layer CLT
- 2. HAAS (2006): full scale fire tests on timber-houses with a light-weightroof and with a timber solid construction roof (CLT)
- 3. SOFIE (2007): full scale fire test on a 3-storey-building (see A. Ceccotti)
- 4. CLT-FIRE hbf-TUG-ETHZ (2009): first parameter studies during fire-tests on CLT
- Current: Fire tests in Sweden/SP Trätek PhD work startet at ETH



1. Bresta H – KLH (1998): fire-bending tests on loaded 5-layer CLT







# 2. HAAS (2006): full scale fire tests

Timber Light-weight Construction **TLC** 



### Timber Solid Construction TSC



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# **Fire Research on CLT**



#### Timber Solid Construction **TSC**

![](_page_13_Picture_5.jpeg)

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![](_page_14_Picture_1.jpeg)

# 2. HAAS (2006): full scale fire tests

Timber Light-weight Construction **TLC** 

![](_page_14_Picture_5.jpeg)

#### Timber Solid Construction **TSC**

![](_page_14_Picture_7.jpeg)

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# **Fire Research on CLT**

# 2. HAAS (2006): full scale fire tests

Timber Light-weight Construction **TLC** 

![](_page_15_Picture_5.jpeg)

### Timber Solid Construction **TSC**

![](_page_15_Picture_7.jpeg)

![](_page_16_Picture_0.jpeg)

# tudy research engineering test center Introduction | History

# **Fire Research on CLT**

# 3. SOFIE (2007): full scale fire test on a 3-storey-building (see A. Ceccotti)

![](_page_16_Picture_4.jpeg)

![](_page_17_Picture_1.jpeg)

 CLT-FIRE hbf-TUG-ETHZ (2009): first parameter studies during fire-tests on CLT
 Parameters - glue, thickness of layers, orientation

	10/10/10/10/20	20/20/20	30/30 Trägerplatte
PUR-1	X		X
PUR-2	X		
PUR-3	X	X	
PUR-4	X	X	
PUR-5		X	
MUF	X		X

### 1 specimen with 5-layered uni-directional cross section and PUR

![](_page_18_Picture_1.jpeg)

4. CLT-FIRE hbf-TUG-ETHZ (2009): first parameter fire-tests on CLT

# Parameters - glue, thickness of layers, orientation

	Trögerplatte	Trägerplatte	Trägerplatte
PUR-1	Х		Х
PUR-2	Х		
PUR-3	Х	Х	
PUR-4	Х	Х	
PUR-5		Х	
MUF	Х		X

1 specimen with 5-layered unidirectional cross section and PUR Determination of charring rate and charring depth via temperature with thermocouples placed between the single layers

![](_page_18_Picture_8.jpeg)

![](_page_19_Picture_1.jpeg)

# **1K-PUR: Oberservations during fire tests**

![](_page_19_Picture_4.jpeg)

![](_page_20_Picture_1.jpeg)

# **MUF: Oberservations during fire tests**

![](_page_20_Picture_4.jpeg)

![](_page_20_Picture_5.jpeg)

![](_page_20_Picture_6.jpeg)

Charred layers do not fall off – thermal insulation as known from sawn timber and GLT is given

![](_page_21_Picture_1.jpeg)

# **1K-PUR: charring depth**

![](_page_21_Figure_4.jpeg)

⇒ Effect due to different 1K-PUR glues regarding charring rates may be neglected.

![](_page_22_Picture_1.jpeg)

# Charring – Parameter GLUE – 1K-PUR / MUF

![](_page_22_Figure_4.jpeg)

⇒ Type of glue (PUR – MUF) has a significant influence on the charring behaviour

![](_page_23_Picture_1.jpeg)

# EN 1995-1-2:

Difference between unprotected

and initial protected timber cross sections.

![](_page_23_Figure_6.jpeg)

![](_page_24_Picture_1.jpeg)

# Proposal to EN 1995-1-2 for the design of CLT

- Cross sections with 1-K PUR → initial protected timber
- Cross sections with MUF → unprotected timber

![](_page_24_Figure_6.jpeg)

![](_page_25_Picture_1.jpeg)

# Proposal to EN 1995-1-2 for the design of CLT

- Cross sections with 1-K PUR → initial protected timber
- Cross sections with MUF → unprotected timber

![](_page_25_Figure_6.jpeg)

![](_page_26_Picture_1.jpeg)

# **Comparison between proposal and test results**

![](_page_26_Figure_4.jpeg)

![](_page_27_Picture_2.jpeg)

![](_page_27_Figure_3.jpeg)

2-layer specimen MUF

![](_page_27_Figure_5.jpeg)

![](_page_27_Figure_6.jpeg)

-10

![](_page_28_Picture_0.jpeg)

![](_page_28_Picture_1.jpeg)

#### Proposal for design: Difference between PUR an MUF for R30

![](_page_28_Figure_3.jpeg)

### No difference between PUR and MUF!

![](_page_29_Picture_0.jpeg)

### Proposal for design: Difference between PUR an MUF for R60

![](_page_29_Figure_4.jpeg)

### **Difference between PUR and MUF 5 mm!**

![](_page_30_Picture_0.jpeg)

![](_page_30_Picture_1.jpeg)

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